



# **A Single Phase High Power Factor AC-DC converter with Soft Switching Characteristics**

Neethu Venugopal<sup>1</sup>, Nimmy George<sup>2</sup>

PG Student [PE], Dept. of EEE, Sree Narayana Gurukulam College of Engineering, Kadayiruppu, Kerala, India<sup>1</sup>

Assistant Professor, Dept. of EEE, Sree Narayana Gurukulam College of Engineering, Kadayiruppu, Kerala, India<sup>2</sup>

**ABSTRACT:** This paper proposes an integrated high power factor ac-dc converter with soft switching characteristics. The circuit consists of a buck converter and a boost converter that integrates to form the proposed circuit topology. The boost converter operates in discontinuous-conduction mode (DCM) to perform the function of high power factor correction (PFC). The buck converter regulates the output voltage of the boost converter to supply stable dc voltage to the load. Both converters operate at high switching frequency. The active switches of the proposed converter operates at DCM for achieving zero-voltage switch-on(ZVS).The low-pass filter is used to remove the high frequency ripples of current. Circuit configuration and the circuit operation for eight modes explained. The simulink model of the proposed circuit provided.

**KEYWORDS:** Boost converter, Buck converter, Discontinuous-conduction mode (DCS), Zero-voltage switch-on, Power factor correction (PFC).

## **I.INTRODUCTION**

Ac/dc converters have been widely used in many applications such as LED lighting systems, industrial drives, electric power distribution systems, telecommunication systems, energy conversion systems and other high power applications. The boost, buck-boost converters have been widely used as power factor correctors. The most popular topology in power factor correction application is the boost topology. A boost converter or step up converter is a power dc to dc converter with an output dc voltage which is greater than output dc voltage. The boost topology is simple, and it allows low distorted input currents and an almost unity power factor with different control techniques. At low line input, the switch conduction losses are high, because the input RMS current has the highest value and the highest step-up conversion is required. The inductor has to be over sized for large RMS currents at a low line input, and for the highest volt-seconds applied throughout the input-line range. As a result, a boost converter designed for universal-input PFC applications is heavily oversized, compared to a converter designed for a narrow range of input line voltages. Due to large energy storage filter capacitor at the output, the boost converter has inrush current problems that can be mitigated by using additional components. Here the boost converter performs the function of PFC to obtain high power factor and low current harmonics at the input line. The buck converter further regulates the dc-link voltage to provide a stable dc output voltage.

Hard switching operation of active switches causes many problems in the circuit. This generates high switching losses and introduces high voltage and current stresses on circuit components. The circuit efficiency and stability decreases. In the proposed circuit both active switches are turned on at ZVS. It assures high circuit efficiency and stability. PI control method is used in the proposed circuit.

## **II.CIRCUIT MODEL**

The circuit topology is derived by integrating a boost converter and buck converter. The proposed circuit consists of a low-pass filter circuit, a diode-bridge rectifier, a boost converter, a buck converter. The buck converter is composed of  $L_b$ ,  $D_s$ ,  $D_{S2}$ ,  $S_1$  and  $C_0$ . The boost converter is composed of  $L_p$ ,  $D_{S1}$ ,  $S_2$  and  $C_{dc}$ . Both converters operate at a high-switching frequency. The boost converter performs the function of power factor correction (PFC) to obtain high power factor at input line. When the boost converter operates at discontinuous-conduction mode (DCM), the average value of its inductor current in every high-switching cycle is approximately a sinusoidal function. The low-pass filter is used to

# International Journal of Advanced Research in Electrical, Electronics and Instrumentation Engineering

(An ISO 3297: 2007 Certified Organization)

Vol. 5, Issue 3, March 2016

remove the high frequency current of the inductor current. The input line current becomes sinusoidal and in phase with the input line voltage. So that high power factor can be achieved. The buck converter regulates the output voltage of boost converter to supply stable dc voltage to the load. In order to prevent both the active switches conducting at same time, there is a short non-overlap time defined as “dead time”.



Fig. 1 Proposed ac/dc converter circuit topology

The proposed circuit shown in figure 1 consists of a low-pass filter circuit, a diode-bridge rectifier, a boost converter, a buck converter.

### III. CIRCUIT OPERATION

The circuit operation of the proposed circuit can be described in eight operation modes.

a) Mode 1

Prior to mode 1,  $S_1$  is at “ON” state. Boost inductor current  $I_p$  is zero. The dc-link capacitor supplies the buck inductor current  $I_b$  which flows through  $S_1$ ,  $D_5$ ,  $L_b$ , and  $C_0$ . This mode starts when  $S_1$  is turned off by the gate voltage  $V_{GS1}$ . At the beginning of this mode,  $I_b$  is diverted from  $S_1$  to flow through the output capacitors  $C_{DS1}$  and  $C_{DS2}$ .  $C_{DS1}$  charged and  $C_{DS2}$  discharged. As the voltage across  $C_{DS2}$ , that is  $V_{DS2}$  decreases to be lower than the rectified input voltage  $V_{rec}$ , then the boost inductor current  $I_p$  starts to increase. When  $V_{DS2}$  equals to  $-0.7V$ ,  $D_{S2}$  turns on and mode 1 ends.

b) Mode 2

At the beginning of mode 2,  $V_{DS2}$  maintained at about “ $-0.7V$ ” by antiparallel diode  $D_{S2}$ . After short dead time,  $S_2$  is turned on by the gate voltage  $V_{GS2}$ . The on resistance of  $S_2$  is small enough, most of  $I_b$  will flow through  $S_2$  from source to drain. In this mode  $I_b$  is greater than  $I_p$ ,  $I_b$  keep decreases and  $I_p$  increases from zero, since boost converter designed to operate in DCM.  $I_b$  has two loops. A part of  $I_b$  flows through  $S_2$ , rest are equal to  $I_p$  that flows through the line voltage source, diode rectifier and  $L_p$ . This mode ends when  $I_p$  is greater than  $I_b$ .

c) Mode 3

In this mode  $I_p$  is greater than  $I_b$ .  $I_p$  has two loops. A part of  $I_p$  flows through  $S_2$  so the direction of current flow naturally changes. Current flows from drain to source. The rest flows through buck converter, equals to  $I_b$ . In this mode  $I_b$  keep decreases and  $I_p$  increases. This mode ends when  $I_b$  equals to zero, since buck converter designed to operate at DCM.

# International Journal of Advanced Research in Electrical, Electronics and Instrumentation Engineering

(An ISO 3297: 2007 Certified Organization)

Vol. 5, Issue 3, March 2016

d) Mode 4

In this mode  $S_2$  remains on to carry  $I_p$ . Because of  $I_b$  is zero, the buck converter is at off state. Here  $I_p$  increases. The output capacitor  $C_0$  supplies current to load. This mode ends when  $S_2$  is turned off by  $V_{GS2}$ .

e) Mode 5

At the beginning of this mode  $I_b$  equals to zero. Current  $I_p$  reaches maximum when  $S_2$  turned off.  $I_p$  will be diverted from  $S_2$  to flow through  $C_{DS1}$  and  $C_{DS2}$ .  $C_{DS1}$  discharged and  $C_{DS2}$  charged. As the voltage across  $C_{DS1}$  decreases to be lower than  $V_{dc}-V_0$  then  $I_b$  start to increase so that voltage across  $L_b$  becomes positive. When  $V_{DS1}$  equals to  $-0.7V$ ,  $D_{S1}$  turns on and this mode ends.

f) Mode 6

At the beginning of this mode,  $V_{DS1}$  maintained to about  $-0.7V$  by antiparallel diode  $D_{S1}$ . After short dead time,  $S_1$  is turned on by  $V_{GS1}$ . On resistance of  $S_1$  is small enough, so that rest of  $I_p$  will flows through  $S_1$  in the direction from source to drain. In this mode  $I_p$  is greater than  $I_b$ . There are two loops for  $I_p$ . A part of  $I_p$  flows through  $S_1$  to charge dc link capacitor. The rest are equals to  $I_b$ , flows into buck converter. This mode ends when  $I_b$  is greater than  $I_p$ .

g) Mode 7

In this mode  $I_b$  is greater than  $I_p$ . Current  $I_p$  keep decreases and current  $I_b$  keep increases.  $I_b$  has two loops. A part of  $I_b$  flows through  $S_1$ , the direction naturally changed so that from drain to source. The rest flows through boost converter. This mode ends when current  $I_p$  becomes zero.

h) Mode 8

In this mode  $S_1$  remains on and  $I_b$  keeps increasing. This mode ends at the time when  $V_{GS1}$  becomes a low level to turn off  $S_1$ . The circuit operation returns to mode1.

## IV.SIMULATION

The simulink model of the proposed circuit for an open loop control is as shown in the figure 2. The output voltage waveform obtained is shown in the figure 3.

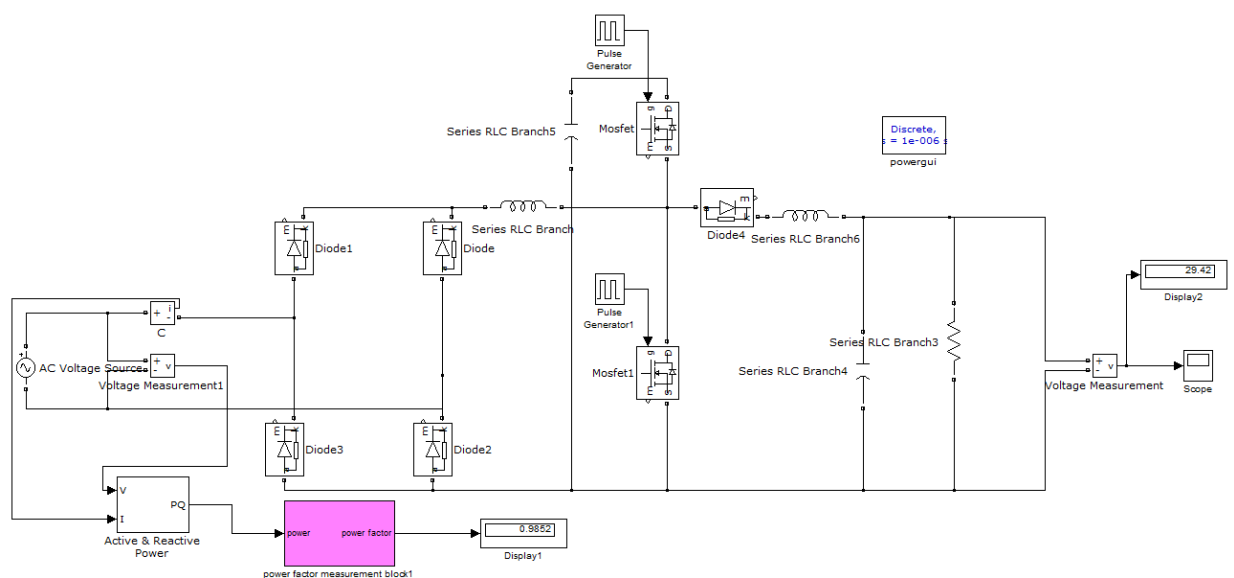


Fig. 2 Open loop control for proposed circuit

The boost converter is designed for an input ac voltage of 14V and an output voltage of 30V. Power output is considered to be 9W. Switching frequency taken as 20 KHz. For the buck converter the input voltage considered as

# International Journal of Advanced Research in Electrical, Electronics and Instrumentation Engineering

(An ISO 3297: 2007 Certified Organization)

Vol. 5, Issue 3, March 2016

30V and it designed for 0.20 duty ratio. The open loop control of proposed circuit as shown in the figure 2 gives a PF of 0.9852

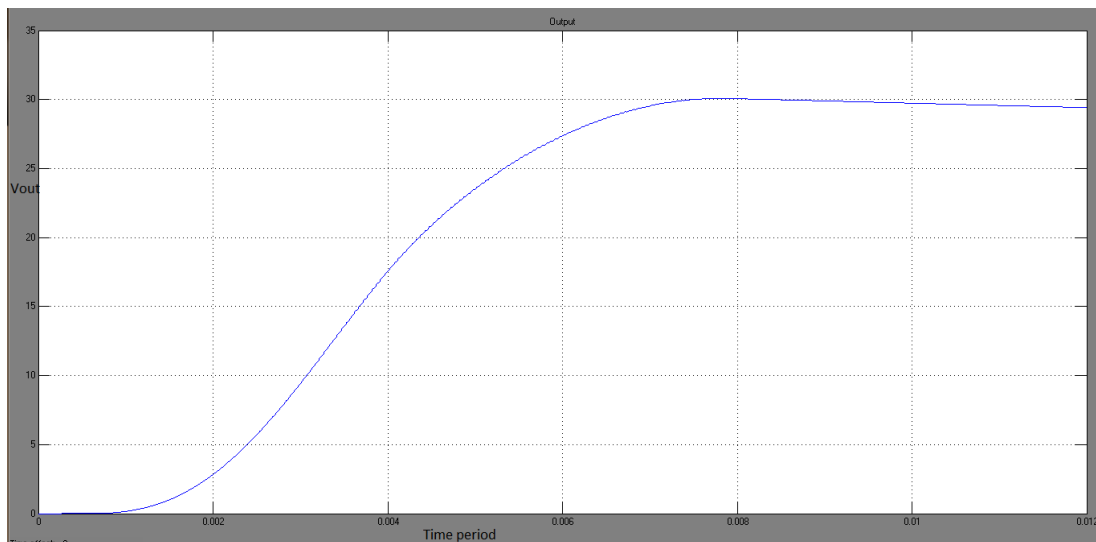


Fig. 3 Output voltage for open loop control circuit

The output voltage waveform obtained is shown in the figure 3. By using open loop control method the output obtained is 29.42V.

The simulink model of the proposed circuit for PI control is as shown in the figure 4. The output voltage waveform obtained is shown in the figure 5. The gate pulse waveform of switches is given in figure 6.

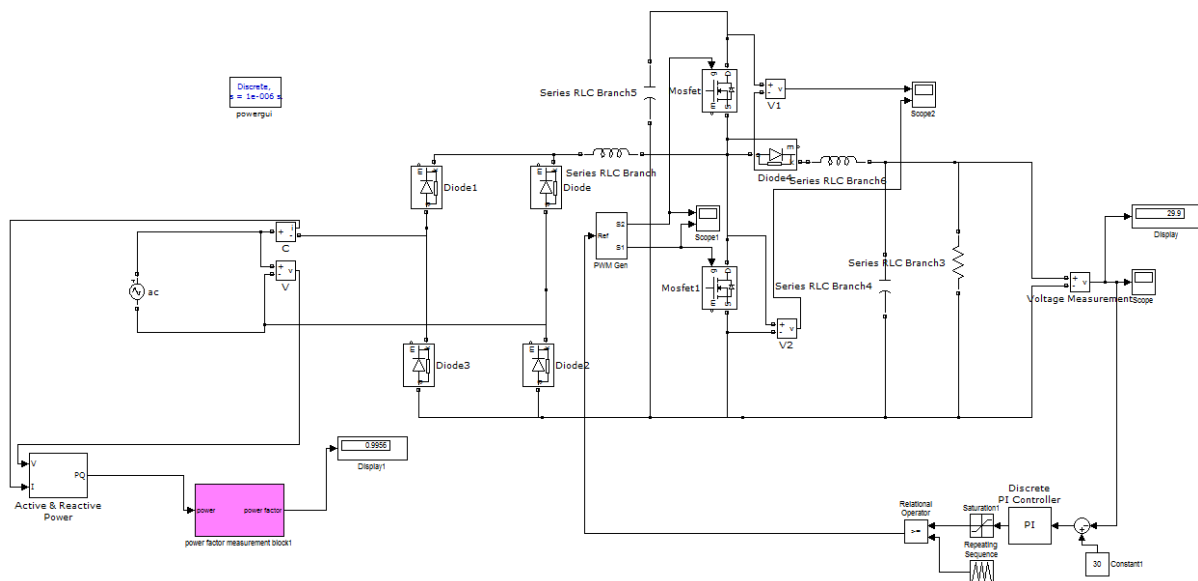


Fig. 4 PI control for proposed circuit

The simulink model of the proposed circuit for PI control is as shown in the figure 4. The boost converter is designed for an input ac voltage of 14V and an output voltage of 30V. Power output is considered to be 9W. Switching frequency taken as 20 KHz. For the buck converter the input voltage considered as 30V and it designed for 0.20 duty ratio.

# International Journal of Advanced Research in Electrical, Electronics and Instrumentation Engineering

(An ISO 3297: 2007 Certified Organization)

Vol. 5, Issue 3, March 2016

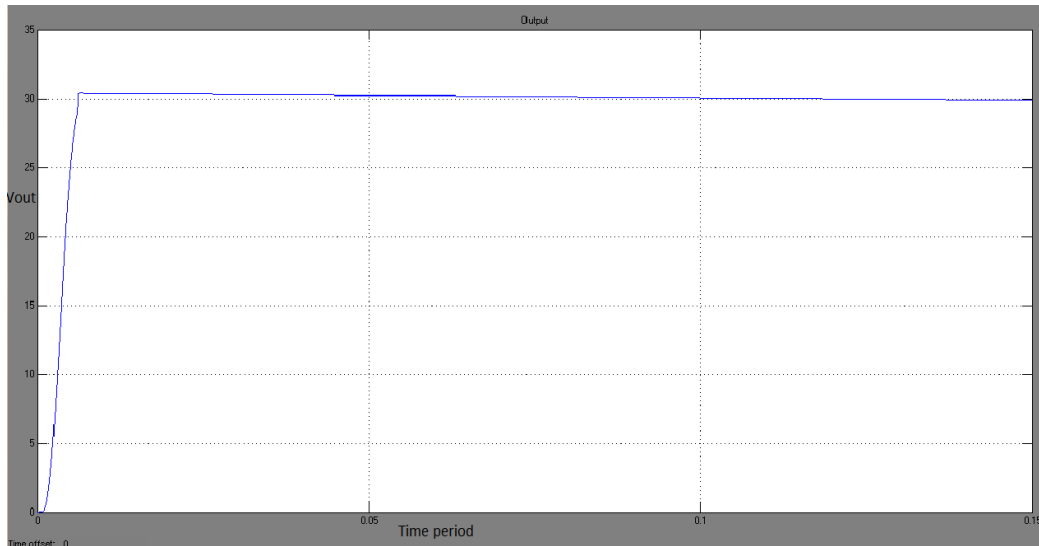


Fig. 5 Output for the PI control circuit

The output voltage obtained for the PI control method is as shown in the figure 5. PI control circuit gives an output voltage of 29.9V.

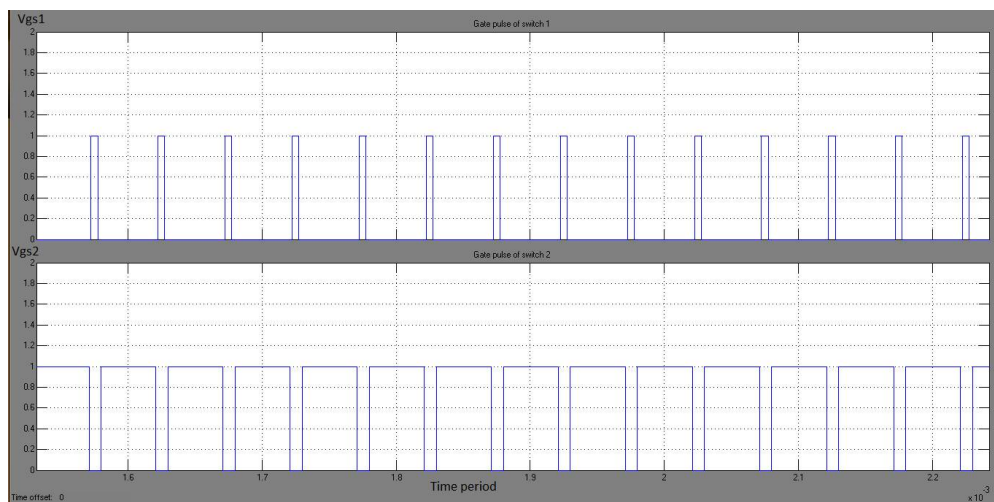


Fig. 6 Gate pulse generated for active switches

The gate pulses generated for the on/off operation of active switches is as shown in the figure 6. There is a short non-overlap time defined as “dead time”.

## V.HARDWARE IMPLEMENTATION

The hardware implementation of the proposed circuit is as shown in the figure 7 The circuit is implemented by using dsPIC30F2010 . LM7805 voltage regulator IC used to regulate the output voltage at 5V. An input from 7.2 to 35 provides a steady value of 5V.

# International Journal of Advanced Research in Electrical, Electronics and Instrumentation Engineering

(An ISO 3297: 2007 Certified Organization)

Vol. 5, Issue 3, March 2016

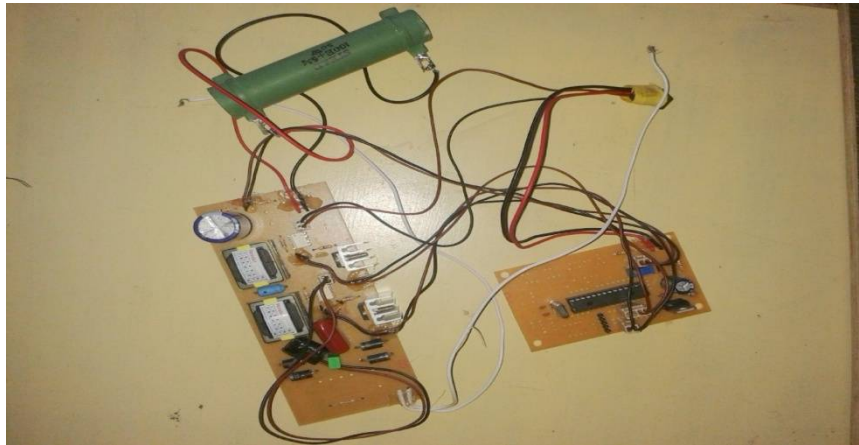


Fig. 7 Proposed circuit hardware

The output waveform obtained is given in figure 8.

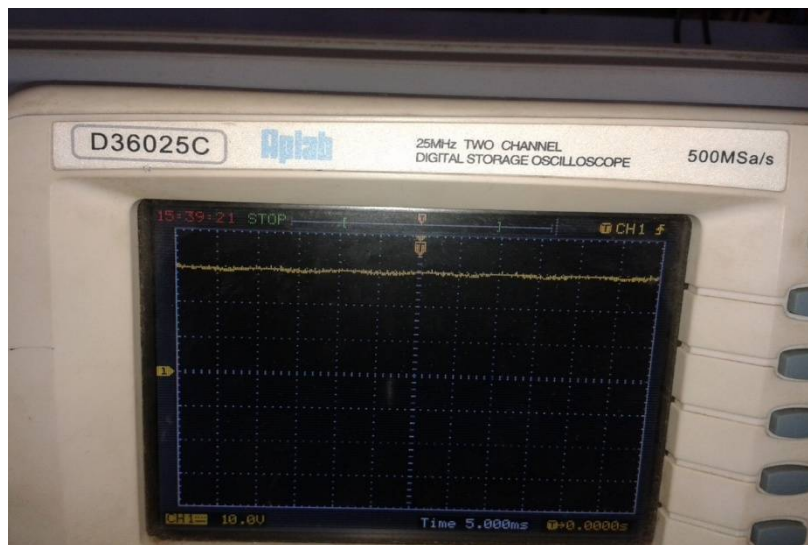


Fig. 8 Output waveform

Output voltage of the proposed circuit is 30V as per the design.

## VI.RESULT

Proposed ac/dc converter is shown in the figure 1. By using open loop control circuit the ac/dc converter is as shown in figure 2, the power factor obtained is 0.9852. The circuit gives an output voltage of 29.42V. The output voltage waveform is given in figure 3. The proposed converter use PI control method as shown in figure 4. In the case of PI control the proposed circuit gives power factor of 0.9956 and the output voltage is 29.9V. The output voltage waveform is given in the figure 5. So PI closed loop control method is used in the ac/dc converter. The figure 6 shows gate pulses generated for the active switches that ensure dead time. The PI control assures high circuit efficiency and high power factor. The hardware implementation of the proposed circuit is given in figure 7. It provides an output voltage of 30V. The output voltage waveform is as shown in the figure8.

## VII.CONCLUSION

The proposed circuit topology gives a high efficiency zero voltage switching ac/dc converter. It integrates a boost converter and a buck converter. Zero voltage switching achieved by freewheeling the inductor currents of converters



# International Journal of Advanced Research in Electrical, Electronics and Instrumentation Engineering

(An ISO 3297: 2007 Certified Organization)

Vol. 5, Issue 3, March 2016

through the intrinsic diodes of the MOSFETs. The boost converter performs the function of power factor correction. For the purpose boost converter is designed to operate at DCM. The buck converter in the circuit regulates the dc-link voltage to provide stable dc output voltage.. The proposed circuit is controlled by PI control method. It provides high power factor and assures circuit efficiency.

## REFERENCES

- [1] C. M. Wang, C. H. Lin, and T. C. Yang, "High-power-factor soft-switched dc power supply systems," IEEE Trans. Power Electron., vol. 26, no. 2, pp. 647-654, Feb. 2011.
- [2] J. M. Alonso, J. Vina, D. G. Vaquero, G. Martinez, and R. Osorio, "Analysis and design of the integrated double buck-boost converter as a high-power-factor driver for power-LED lamps," IEEE Trans. Ind. Electron., vol. 59, no. 4, pp. 1689-1697 April 2012,.
- [3] R. T. Chen and Y. Y. Chen, "Single stage push pull boost converter with integrated magnetic and input current shaping technique," IEEE Trans. Power Electron., vol. 21, no. 5, pp. 1193-1203, Sep. 2006.
- [4] M. Z. Youssef, and P. K. Jain, "A novel single stage AC-DC self oscillating series-parallel resonant converter," IEEE Trans. Power Electron., vol. 21, no. 6, pp. 1735-1744, Nov. 2006.
- [5] K. W. Seok, and B. H. Kwon, "A novel single-stage half-bridge ac-dc converter with high power factor," IEEE Trans. Ind. Electron., vol. 48, no. 6, pp. 1219-1225, Dec. 2001.
- [6] S. S. Lee, S. W. Choi, and G. W. Moon, "High-efficiency active-clamp forward converter with transient current build-up (TCP) ZVS technique," IEEE Trans. Ind. Electron., vol. 54, no. 1, pp. 310-318, Feb. 2007.
- [7] D. L. O'Sullivan, M. G. Egan, and M. J. Willers, "A family of single stage resonant ac/dc converters with PFC," IEEE Trans. Power Electron., vol. 24, no.2, pp. 398-408, Feb. 2009.
- [8] J. W. Yang and H. L. Do, "High-efficiency ZVS AC-DC LED driver using a self-Driven synchronous rectifier," IEEE Trans. Circuits and Systems –I: Regular Papers, vol. 61, no. 8, pp. 2505-2512, Aug. 2014.
- [9] M. Marvi and A. Fotowat-Ahmady, "A fully ZVS critical conduction mode boost PFC," IEEE Trans. Power Electron., vol. 27, no.4 pp.1958-1965, April 2012.